

ARCH 631. Formulas of Exam 2
from Lectures, Examples, and Assignments

$\sum F_x = 0$	$\sum F_y = 0$	$\sum M = 0$	
$V = \int -w dx$	$M = \int V dx$	$M = Fd$	
area of a rectangle = $b \times h$	area of a triangle = $\frac{b \times h}{2}$	area of a trapezoid = $b \times \frac{(h_1 + h_2)}{2}$	
fixed base portal frame with assumed inflection points and lateral load: $R_{1x} = R_{2x} = \frac{P}{2}$ $R_{1y} = -0.45 \frac{Ph}{L}$ $R_{2y} = 0.45 \frac{Ph}{L}$ $M_1 = M_2 = 0.275 Ph$ $M_{joints} = 0.225 Ph$	$f_{max} = \frac{P}{A} + \frac{Mc}{I} = \frac{P}{A} + \frac{M}{S}$	three span beam with integral end supports: $V_{max} = 1.15 \frac{wL}{2}$ $M_{max+ends} = \frac{wL^2}{14}$ $M_{max+interior} = \frac{wL^2}{16}$ $M_{max-column} = \frac{wL^2}{16}$ $M_{max-ends, other support} = \frac{wL^2}{10}$ $M_{max-interior} = \frac{wL^2}{11}$	
	$w = \gamma A$		
	simply supported at corners square plate $m_{max} = 0.15 w' a^2$		
	2. $1.2D + 1.6L$		
$M = Td$	slab depth = $\frac{L}{\text{number}}$ or $\frac{\ell_n}{\text{number}}$		
$\ell_n = \ell - \frac{1}{2} \text{ support 1 width} - \frac{1}{2} \text{ support 2 width}$	$m = \frac{M}{\text{strip width}}$	$M_o = (M_T) = \frac{w_u \ell_n^2}{8}$	
flat slab, interior bay, COLUMN strip: $M_{negative} = (0.75 \cdot 0.65 M_T) = 0.49 M_o$ $M_{positive} = (0.60 \cdot 0.35 M_T) = 0.21 M_o$ flat slab, interior bay, MIDDLE strip: $M_{negative} = (0.25 \cdot 0.65 M_T) = 0.16 M_o$ $M_{positive} = (0.40 \cdot 0.35 M_T) = 0.14 M_o$	fully fixed square plate $m_{negative} = 0.0513 w' a^2$	$\phi M_n = \phi A_s f_y \left(d - \frac{a}{2} \right) \quad \phi = 0.9^*$	
	$a = \frac{A_s f_y}{0.85 f'_c b}$	to determine maximum steel for 0.005 strain $c = 0.375d, \quad a = \beta_1 c$	
	$M_{max(case 1)} = \frac{wl^2}{8}$	$R_n = \frac{M_n}{bd^2}$ or $\frac{M_u}{\phi bd^2}$	
	$\rho = \frac{A_s}{bd}$	$V_{x(case 1)} = \frac{wl}{2} - wx$	
beam: $A_{s-min} = \frac{3\sqrt{f'_c}}{f_y} (b_w d)$ not less than $\frac{200}{f_y} (b_w d)$	$\phi V_c = \phi 2 \lambda \sqrt{f'_c} b_w d \quad \lambda = 1.0$ normal weight		
$\phi V_c \geq V_u > \frac{\phi V_c}{2} : s_{required} = \text{smaller of } \frac{A_v f_{yt}}{50 b_w} \text{ and } \frac{A_v f_{yt}}{0.75 \sqrt{f'_c} b_w}$		$V_u \leq \phi V_c + \phi V_s \quad \phi = 0.75$	
$V_u > \phi V_c : s_{required} = \frac{\phi A_v f_{yt} d}{V_u - \phi V_c}$ or $\frac{\phi A_v f_{yt} d}{\phi V_s}$	$P = f \cdot A$	sphere: $T = p_r \frac{R}{2}$	
$N_\phi = \frac{Rw}{1 + \cos \phi}$	$T = N_\phi \cos \phi a$	cylinder: $T = p_r R$	
$N_\theta = Rw \left(-\frac{1}{1 + \cos \phi} + \cos \phi \right)$	$a = R \sin \phi$	$w = \gamma t$	$f = \frac{T}{t}$
single overhang at 0.292L: $M = 0.043 wL^2$	double overhangs at 0.21L: $M = 0.021 wL^2$	$f_\phi = \frac{N_\phi}{t}$	$f_\theta = \frac{N_\theta}{t}$

$P_o = 0.85f'_c(A_g - A_{st}) + f_y A_{st}$	$L_{LL} = L_o \left(0.25 + \frac{15}{\sqrt{K_{LL} A_T}} \right)$	slabs: $A_{s-min} = 0.002bt$ (40 or 50 grade) $A_{s-min} = 0.0018bt$ (60 grade)
ties: $\phi_c P_n = \phi_c (0.8P_o) \phi_c = 0.65$	$V_{u2} = w_u (\text{tributary area} - b_1 \times b_2)$	$V_{u2} \leq \phi \left(2 + \frac{4}{\beta_c} \right) \lambda \sqrt{f'_c} b_o d \leq \phi 4 \lambda \sqrt{f'_c} b_o d$
spiral: $\phi_c P_n = \phi_c (0.85P_o) \phi_c = 0.75$	$b_E = \min \left(\frac{\ell_n}{4}, b_w + 16t, \text{ or center-center spacing} \right)$	$b_o = 2(b_1) + 2(b_2)$
$E_c = 57,000 \sqrt{f'_c}$ normal weight		