

**Examples:  
Wind Loading**

Example 1

Given the structure with three shear walls and rigid roof diaphragm, determine the horizontal shear distributed to the walls (and piers) with a static wind pressure and the overturning moment on each wall. The basic wind speed for the College Station area is 115 mph from ASCE-7.

Wind Pressure:

Flat roof (0°)

Zone A: 10% of 5 m = 0.5 m

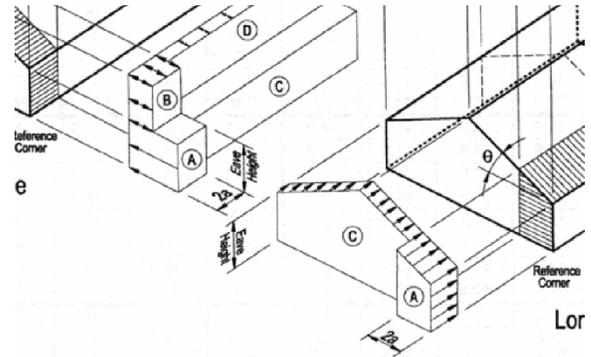
Zone C (~10 ft height)

for simplicity use C

$$p_{s30} = 13.9 \text{ psf}$$

$$\times 0.0479 \text{ kN/m}^2/\text{psf}$$

$$= 0.67 \text{ kN/m}^2 \text{ (KPa)}$$



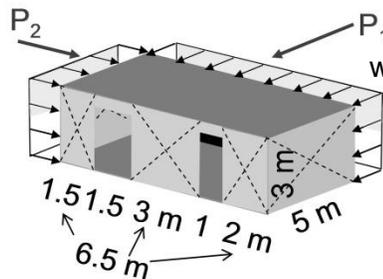
**Simplified Design Wind Pressure ,  $p_{s30}$  (psf) (Expo**

Basic Wind Speed (mph)	Roof Angle (degrees)	Load Case	Zones					
			Horizontal Pressures				Vert	
			A	B	C	D	E	F
115	0 to 5°	1	21.0	-10.9	13.9	-6.5	-25.2	-1.1
	10°	1	23.7	-9.8	15.7	-5.7	-25.2	-1.1
	15°	1	26.3	-8.7	17.5	-5.0	-25.2	-1.1
	20°	1	29.0	-7.7	19.4	-4.2	-25.2	-1.1
	25°	1	26.3	4.2	19.1	4.3	-11.7	-1.1
		2	-----	-----	-----	-----	-4.4	-8.0
	30 to 45	1	23.6	16.1	18.8	12.9	1.8	-1.1
		2	23.6	16.1	18.8	12.9	9.1	-7.0

(Found in Note Set 15.2)

SOLUTION:

The wind pressure needs to be turned into a static force by multiplying by the tributary area, which is half way from other "support" to "support" or top of parapet:



$$w = 0.67 \text{ kPa}$$

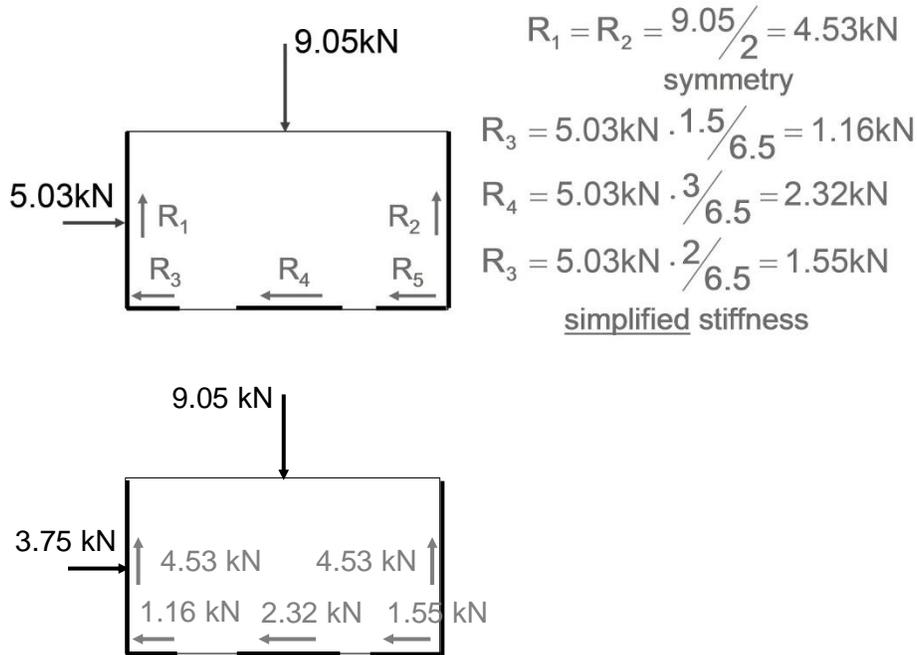
$$P_1 = w \cdot \frac{h}{2} \cdot l = 0.67 \cdot 1.5 \cdot 9 = 9.05 \text{ kN}$$

$$P_2 = w \cdot \frac{h}{2} \cdot d = 0.67 \cdot 1.5 \cdot 5 = 5.03 \text{ kN}$$

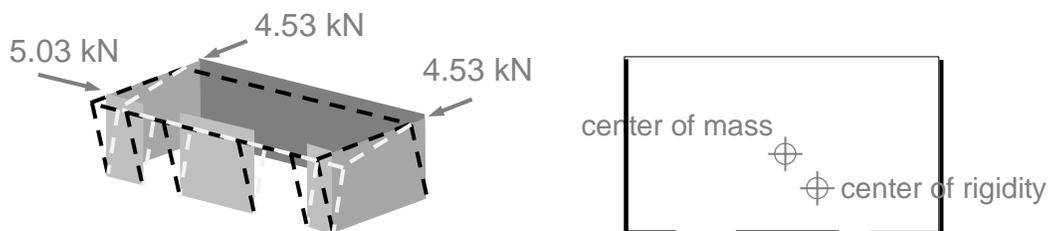
Example 1 (continued)

The force along the wide length,  $P_1$ , can be evenly resisted (split) by the end shear walls because they are the same size and stiffness.

In the long direction, the force  $P_2$  must be resisted by the piers on one side only. The force should be distributed to each pier based on their stiffnesses (a function of  $h/L$ ), but the calculation is laborious. This example splits the force proportionally by length.

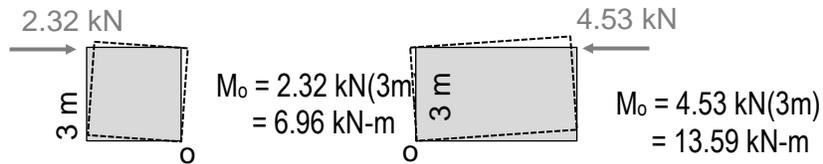


Would this want to twist? A torsional moment will result if the **center of rigidity**, which is the resulting location of the moments of the wall rigidities, does not coincide with the **center of mass** determined from the moments of the wall weight. There is, in effect, an eccentricity.



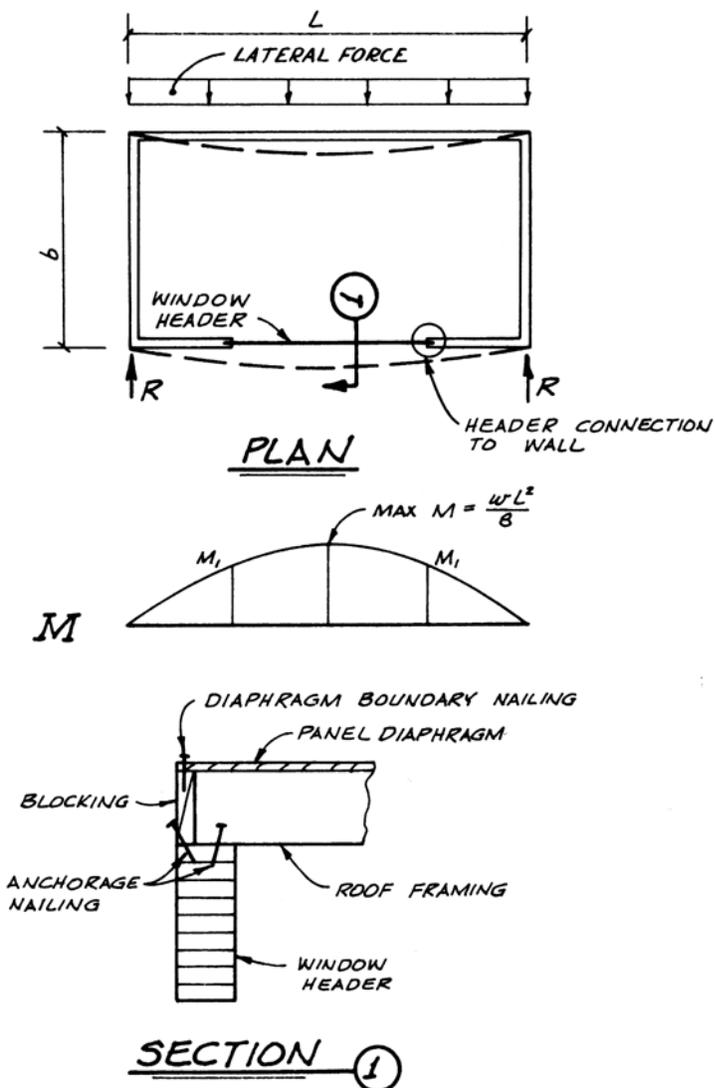
Example 1 (continued)

The overturning moments from the lateral forces at the top of the walls and piers about their bases (or toe) can be calculated.



Example 2

**EXAMPLE 9.7 Header Acting as a Chord**



**Figure 9.9** The header over an opening in a wall may be used as horizontal diaphragm chord.

Example 2 (continued)

Over the window the header serves as the chord. It must be capable of resisting the maximum chord force in addition to gravity loads. The maximum chord force is

$$T = C = \frac{\text{max. } M}{b}$$

The connection of the header to the wall must be designed for the chord force at that point:

$$T_1 = C_1 = \frac{M_1}{b}$$

NOTE: For simplicity, the examples in this book determine the chord forces using the dimension  $b$  as the width of the building. Theoretically  $b$  is the dimension between the centroids of the diaphragm chords, and the designer may choose to use this smaller, more conservative dimension.