Wood Design

Notation:

\(a\) = name for width dimension

\(A\) = name for area

\(A_{req'd - adj}\) = area required at allowable stress when shear is adjusted to include self weight

\(b\) = width of a rectangle

\(c_1\) = coefficient for shear stress for a rectangular bar in torsion

\(C_C\) = curvature factor for laminated arches

\(C_D\) = load duration factor

\(C_{fu}\) = flat use factor for other than decks

\(C_F\) = size factor

\(C_H\) = shear stress factor

\(C_i\) = incising factor

\(C_L\) = beam stability factor

\(C_M\) = wet service factor

\(C_p\) = column stability factor for wood design

\(C_r\) = repetitive member factor for wood design

\(C_V\) = volume factor for glue laminated timber design

\(C_t\) = temperature factor for wood design

\(d\) = name for depth

\(d_{min}\) = dimension of timber critical for buckling

\(DL\) = shorthand for dead load

\(E\) = modulus of elasticity

\(f\) = stress (strength is a stress limit)

\(f_b\) = bending stress

\(f_{from\ table}\) = tabular strength (from table)

\(f_p\) = bearing stress

\(f_r\) = radial stress for a glulam timber

\(f_v\) = shear stress

\(f_{v-max}\) = maximum shear stress

\(F_b\) = tabular bending strength

\(F_{max}\) = maximum internal bending moment

\(F_{max-adj}\) = maximum bending moment adjusted to include self weight

\(F^*\) = intermediate compressive stress for column design dependent on load duration

\(F_{c,E}\) = theoretical allowed buckling stress

\(F_{c,d}\) = tabular compression strength perpendicular to the grain

\(F_p\) = tabular bearing strength parallel to the grain

\(h\) = height of a rectangle

\(I\) = moment of inertia with respect to neutral axis bending

\(I_{trial}\) = moment of inertia of trial section

\(I_{req'd}\) = moment of inertia required at limiting deflection

\(I_y\) = moment of inertia with respect to an y-axis

\(J\) = polar moment of inertia

\(K_{c,E}\) = material factor for wood column design

\(L_e\) = effective length that can buckle for column design, as is \(l_e\)

\(L\) = name for length or span length

\(LL\) = shorthand for live load

\(L_{RFBD}\) = load and resistance factor design

\(M\) = internal bending moment

\(M_{max}\) = maximum internal bending moment

\(M_{max-adj}\) = maximum bending moment adjusted to include self weight

\(P\) = name for axial force vector

\(R\) = radius of curvature of a deformed beam

\(S\) = section modulus

\(S_{req'd}\) = section modulus required at allowable stress
Wood or Timber Design

Structural design standards for wood are established by the National Design Specification (NDS) published by the National Forest Products Association. There is a combined specification (from 2005) for Allowable Stress Design and limit state design (LRFD).

Tabulated wood strength values are used as the base allowable strength (ASD) and modified by appropriate adjustment factors:

\[
f = C_D C_M C_T C_L C_F \ldots \times f_{\text{from table}}
\]

### Adjustment Factors

- **C_D** load duration factor
- **C_M** wet service factor
  
  \(1.0 \text{ dry} < 16\% \text{ moisture content})
- **C_T** temperature factor (at high temperatures strength decreases)
- **C_L** beam stability factor (for beams without full lateral support)
- **C_F** size factor for visually graded sawn lumber and round timber > 12” depth

\[
C_F = (12/d)^{1/6} \leq 1.0
\]

- **C_V** volume factor for glued laminated timber (similar to \(C_F\))
- **C_{fu}** flat use factor (excluding decking)
- **C_r** repetitive member factor (1.15 for three or more parallel members of Dimension lumber spaced not more than 24 in. on center, connected together by a load-distributing element such as roof, floor, or wall sheathing)
- **C_c** curvature factor for glued laminated timber (1.0 straight & cambered)

\[
t/R \leq 1/100 \text{ for hardwoods \& southern pine or 1/125 other softwoods}
\]

\[
C_c = 1 - 2000(t/R)^2
\]

- **C_i** incising factor (0.85 incised sawn lumber, 1 for sawn lumber not incised and glulam)
- **C_H** shear stress factor (amount of splitting)
- **C_P** column stability factor (1.0 for fully supported columns)
Design Values

- $F_b$: bending stress
- $F_t$: tensile stress
- $F_v$: horizontal shear stress
- $F_c\perp$: compression stress (perpendicular to grain)
- $F_c\parallel$: compression stress (parallel to grain)
- $E$: modulus of elasticity
- $F_p$: bearing stress (parallel to grain)

Wood is significantly weakest in shear and strongest along the direction of the grain (tension and compression).

Load Combinations and Deflection

The critical load combination is determined by the largest of either:

\[
\frac{\text{dead load}}{0.9} \quad \text{or} \quad \left( \frac{\text{dead load} + \text{any combination of live load}}{C_D} \right)
\]

The deflection limits may be increased for less stiffness with total load: $\text{LL} + 0.5(DL)$

Criteria for Beam Design

Allowable normal stress or normal stress from LRFD should not be exceeded:

Knowing $M$ and $F_b$, the minimum section modulus fitting the limit is:

\[
S_{req'd} \geq \frac{M}{F_b}
\]

Besides strength, we also need to be concerned about serviceability. This involves things like limiting deflections & cracking, controlling noise and vibrations, preventing excessive settlements of foundations and durability. When we know about a beam section and its material, we can determine beam deformations.

Determining Maximum Bending Moment

Drawing V and M diagrams will show us the maximum values for design. Computer applications are very helpful.

Determining Maximum Bending Stress

For a prismatic member (constant cross section), the maximum normal stress will occur at the maximum moment.

For a non-prismatic member, the stress varies with the cross section AND the moment.
Deflections

Elastic curve equations can be found in handbooks, textbooks, design manuals, etc...Computer programs can be used as well.

Elastic curve equations can be superpositioned ONLY if the stresses are in the elastic range. The deflected shape is roughly the same shape flipped as the bending moment diagram but is constrained by supports and geometry.

Allowable Deflection Limits

All building codes and design codes limit deflection for beam types and damage that could happen based on service condition and severity.

<table>
<thead>
<tr>
<th>Use</th>
<th>LL only</th>
<th>DL+LL</th>
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</thead>
<tbody>
<tr>
<td>Roof beams:</td>
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<td></td>
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<tr>
<td>Industrial</td>
<td>L/180</td>
<td>L/120</td>
</tr>
<tr>
<td>Commercial</td>
<td></td>
<td></td>
</tr>
<tr>
<td>plaster ceiling</td>
<td>L/240</td>
<td>L/180</td>
</tr>
<tr>
<td>no plaster</td>
<td>L/360</td>
<td>L/240</td>
</tr>
<tr>
<td>Floor beams:</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Ordinary Usage</td>
<td>L/360</td>
<td>L/240</td>
</tr>
<tr>
<td>Roof or floor (damageable elements)</td>
<td>L/480</td>
<td></td>
</tr>
</tbody>
</table>

Lateral Buckling

With compression stresses in the top of a beam, a sudden “popping” or buckling can happen even at low stresses. In order to prevent it, we need to brace it along the top, or laterally brace it, or provide a bigger $I_y$.

Beam Loads & Load Tracing

In order to determine the loads on a beam (or girder, joist, column, frame, foundation...) we can start at the top of a structure and determine the *tributary area* that a load acts over and the beam needs to support. Loads come from material weights, people, and the environment. This area is assumed to be from half the distance to the next beam over to halfway to the next beam.

The reactions must be supported by the next lower structural element *ad infinitum*, to the ground.

Design Procedure

The intent is to find the most light weight member satisfying the section modulus size.

1. Know $F_{all}$ for the material or $F_U$ for LRFD.
2. Draw $V$ & $M$, finding $M_{max}$.
3. Calculate \( S_{\text{req'd}} \). This step is equivalent to determining \( f_b = \frac{M_{\text{max}}}{S} \leq F'_b \)

4. For rectangular beams \( S = \frac{bh^2}{6} \)

   - For timber: use the section charts to find \( S \) that will work and remember that the beam self weight will increase \( S_{\text{req'd}} \).

****Determine the “updated” \( V_{\text{max}} \) and \( M_{\text{max}} \) including the beam self weight, and verify that the updated \( S_{\text{req'd}} \) has been met.******

5. Consider lateral stability.

6. Evaluate horizontal shear stresses using \( V_{\text{max}} \) to determine if \( f_v \leq F'_v \)

   For rectangular beams \( f_{v-\text{max}} = \frac{3V}{2A} = 1.5 \frac{V}{A} \)

7. Provide adequate bearing area at supports: \( f_p = \frac{P}{A} \leq F'_p \)

8. Evaluate shear due to torsion \( f_v = \frac{T_P}{J} \) or \( \frac{T}{c_1ab^2} \leq F'_v \)

   (circular section or rectangular)

9. Evaluate the deflection to determine if \( \Delta_{\text{max,LL}} \leq \Delta_{\text{LL-allowed}} \) and/or \( \Delta_{\text{max,Total}} \leq \Delta_{\text{Total-allowed}} \)

   **** note: when \( \Delta_{\text{calculated}} > \Delta_{\text{limit}} \), \( I_{\text{required}} \) can be found with: \( I_{\text{req'd}} \geq \frac{\Delta_{\text{as big as}}}{\Delta_{\text{limit}}} I_{\text{trial}} \)

   and \( S_{\text{req'd}} \) will be satisfied for similar self weight ******

FOR ANY EVALUATION:

Redesign (with a new section) at any point that a stress or serviceability criteria is NOT satisfied and re-evaluate each condition until it is satisfactory.

**Column Design**


Any slenderness ratio, \( l_e/d \leq 50 \):

\( f_c = \frac{P}{A} \leq F'_c \)

\( F'_c = F_c (C_D)(C_M)(C_I)(C_F)(C_p) \)

For preliminary column design:

\( F'_c = F_c C_p = (F_c C_D)C_p \)
Procedure

1. Obtain $F'_{c}$
   
   find $l \phi /d$ or assume $(l \phi /d \leq 50)$
   
   compute $F_{cE} = \frac{K_{cE} E}{(l \phi /d)^2}$ with $K_{cE} = 0.3$ for sawn, $= 0.418$ for glu-lam
   
   compute $F^*_{c} \approx F_{c} C_{D}$ with $C_{D} = 1$, normal, $C_{D} = 1.25$ for 7 day roof...
   
   find $F_{cE} / F^*_{c}$ and get $C_{p}$

2. Select a section

   If the load and area of the column are known, set the stress equal to the allowable stress, and solve for $l_{e}, l$, or $d_{min}$

   If the load and length of the column are known, set the stress equal to the allowable stress, and solve for $A$ or $d_{min}$ and select a section that satisfies the values found.

3. Continue from 2 until $F'_{c}$ is satisfied: $F'_{c} = F^*_{c} C_{p}$

Alternate Column Allowable Stress

For intermediate length columns with $11 < L/d < \kappa$, where $\kappa = 0.67 \sqrt{E / F_{c}}$:

$$F'_{c} = F_{c} \left[ 1 - \frac{1}{3} \left( \frac{L_{c}}{d} \right) \kappa \right]$$

For long columns with $L/d > \kappa$, and an assumed safety factor of 2.73: the allowable stress is:

$$F_{c} = \frac{0.3E}{\left( L_{c} / d \right)^2}$$
Table 9.3  Column stability factor $C_{p}$

Static and Strength of Materials for Architecture and Building Construction, 2nd ed., Onouye & Kane

**Column Stability Factor $C_{p}$**

<table>
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<tr>
<th>$F_{ck}$</th>
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<th>Glu-Lam</th>
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</tbody>
</table>

Table developed and permission for use granted by Professor Ed Lebert, Dept. of Architecture, University of Washington.
SECTION PROPERTIES/STANDARD SIZES

To the extent that other considerations will permit, the finished sizes of structural glued laminated timber as given in Table 8 constitute normal industry practice. Industry standards do, however, permit the use of any depth or width of glued laminated timber. Dimension lumber of 1½-in. net thickness is normally used for laminating straight members.

The modified section modulus includes size factor (C), and no further reduction of bending stress for size is needed.

| DEPTH, d in. | AREA, A in² | MODIFIED SECTION
| MOODUMENT, SC in³ | DEPTH, d in. | AREA, A in² | MODIFIED SECTION
| MOODUMENT, SC in³ | DEPTH, d in. | AREA, A in² | MODIFIED SECTION
| MOODUMENT, SC in³ | DEPTH, d in. | AREA, A in² | MODIFIED SECTION
| MOODUMENT, SC in³ | DEPTH, d in. | AREA, A in² | MODIFIED SECTION
| MOODUMENT, SC in³ |
| 3⅛" WIDTH |
| 6.0 | 18.8 | 18.8 | 56 | 94.0 | 162.0 | 600.0 | 7.776 |
| 6.5 | 170.1 | 672.8 | 9.397 | 25.5 |
| 7.0 | 182.3 | 749.5 | 11.072 | 27.0 |
| 7.5 | 192.4 | 830.0 | 13.012 | 29.5 |
| 8.0 | 202.5 | 914.5 | 15.188 | 30.0 |
| 8.5 | 212.6 | 1,008.2 | 17.581 | 31.5 |
| 9.0 | 222.7 | 1,102.9 | 20.085 | 33.0 |
| 9.5 | 232.8 | 1,207.6 | 22.672 | 34.5 |
| 10.0 | 242.9 | 1,312.3 | 25.259 | 36.0 |
| 10.5 | 253.0 | 1,417.0 | 27.846 | 37.5 |
| 11.0 | 263.1 | 1,521.7 | 30.434 | 39.0 |
| 11.5 | 273.2 | 1,626.5 | 33.021 | 40.5 |
| 12.0 | 283.3 | 1,731.2 | 35.608 | 42.0 |
| 12.5 | 293.4 | 1,836.0 | 38.195 | 43.5 |
| 13.0 | 303.5 | 1,940.8 | 40.782 | 45.0 |
| 13.5 | 313.6 | 2,045.6 | 43.369 | 46.5 |
| 14.0 | 323.7 | 2,150.4 | 45.956 | 48.0 |
| 14.5 | 333.8 | 2,255.2 | 48.543 | 49.5 |
| 15.0 | 343.9 | 2,360.0 | 51.130 | 51.0 |
| 15.5 | 354.0 | 2,464.8 | 53.717 | 52.5 |
| 16.0 | 364.1 | 2,570.6 | 56.304 | 54.0 |
| 16.5 | 374.2 | 2,676.4 | 58.891 | 55.5 |
| 17.0 | 384.3 | 2,782.2 | 61.478 | 57.0 |
| 17.5 | 394.4 | 2,888.0 | 64.065 | 58.5 |
| 18.0 | 404.5 | 2,993.8 | 66.652 | 60.0 |
| 18.5 | 414.6 | 3,099.6 | 69.239 | 61.5 |
| 19.0 | 424.7 | 3,205.4 | 71.826 | 63.0 |
| 19.5 | 434.8 | 3,311.2 | 74.413 | 64.5 |
| 20.0 | 444.9 | 3,417.0 | 77.000 | 66.0 |
| 20.5 | 455.0 | 3,522.8 | 79.587 | 67.5 |
| 21.0 | 465.1 | 3,628.6 | 82.174 | 69.0 |
| 21.5 | 475.2 | 3,734.4 | 84.761 | 70.5 |
| 22.0 | 485.3 | 3,840.2 | 87.348 | 72.0 |
| 22.5 | 495.4 | 3,946.0 | 89.935 | 73.5 |

| 8⅛" WIDTH |
| 19.0 | 160.0 | 972 | 43.5 | 367.5 | 9.389 | 54.022 | 63.0 |
| 19.5 | 170.1 | 1,076.0 | 11.072 | 54.522 | 7.915 | 62.044 | 72.0 |
| 20.0 | 180.2 | 1,180.0 | 12.755 | 55.522 | 6.438 | 61.066 | 81.0 |
| 20.5 | 190.3 | 1,284.0 | 14.438 | 57.022 | 5.061 | 60.088 | 90.0 |
| 21.0 | 200.4 | 1,388.0 | 16.121 | 58.522 | 3.684 | 59.110 | 99.0 |
| 21.5 | 210.5 | 1,492.0 | 17.804 | 60.022 | 2.307 | 58.132 | 108.0 |
| 22.0 | 220.6 | 1,596.0 | 19.487 | 61.522 | 0.930 | 57.154 | 117.0 |
| 22.5 | 230.7 | 1,699.9 | 21.170 | 63.022 | -0.207 | 56.176 | 126.0 |

| 5⅛" WIDTH |
| 19.0 | 160.0 | 972 | 43.5 | 367.5 | 9.389 | 54.022 | 63.0 |
| 19.5 | 170.1 | 1,076.0 | 11.072 | 54.522 | 7.915 | 62.044 | 72.0 |
| 20.0 | 180.2 | 1,180.0 | 12.755 | 55.522 | 6.438 | 61.066 | 81.0 |
| 20.5 | 190.3 | 1,284.0 | 14.438 | 57.022 | 5.061 | 60.088 | 90.0 |
| 21.0 | 200.4 | 1,388.0 | 16.121 | 58.522 | 3.684 | 59.110 | 99.0 |
| 21.5 | 210.5 | 1,492.0 | 17.804 | 60.022 | 2.307 | 58.132 | 108.0 |
| 22.0 | 220.6 | 1,596.0 | 19.487 | 61.522 | 0.930 | 57.154 | 117.0 |
| 22.5 | 230.7 | 1,699.9 | 21.170 | 63.022 | -0.207 | 56.176 | 126.0 |
Glue Laminated Timber

These members come in nominal widths of 3, 4, 6, 8, 10, 12, 14 and 16 inches. The depth can exceed 12 inches, so the size factor, $C_F$ must be used. The formula is based on a uniformly loaded beam, simply supported with an l/d ratio of 21. With a single midspan load, multiply $C_F$ by 1.078. With two loads at third points, multiply $C_F$ by 0.968. (Note: the table on page 4 provides section modulus that include $C_F$).

$$C_F = (12/d)^{1/6} \leq 1.0$$

If a glulam is subject to lateral buckling, the slenderness factor is used, and the size factor is not.

Bending of a curved glulam causes radial stresses (like membrane pressures) in tension and compression which can be evaluated for an arc with a radius of $R$ at the neutral axis from:

$$f_r = \frac{3M}{2Rbd} \quad \text{for constant rectangular cross section}$$

$$f_r \leq F_R \quad \text{where} \quad F_R = \begin{cases} F_{C\perp} \\ \sqrt{3} F_V \end{cases}$$
ASD Beam Design Flow Chart

1. Collect data: $L$, $\alpha$, $\gamma$, $\Delta_{\text{limits}}$, find beam charts for load cases and $\Delta_{\text{actual}}$ equations.
2. Collect data: $F'_b$ & $F'_v$.
3. Find $V_{\text{max}}$ & $M_{\text{max}}$ from constructing diagrams or using beam chart formulas.
4. Find $S_{\text{req'd}}$ and pick a section from a table with $S_x$ greater or equal to $S_{\text{req'd}}$.
5. Calculate $\omega_{\text{self wt.}}$ using $A$ found and $\gamma$. Find $M_{\text{max-adj}}$ & $V_{\text{max-adj}}$.
   - If $S_{\text{picked}} \geq S_{\text{req'd-adj}}$? (OR calculate $f_b$ Is $f_b \leq F'_b$?)
     - Yes
     - Calculate $A_{\text{req'd-adj}}$ using $V_{\text{max-adj}}$.
       - If $A_{\text{picked}} \geq A_{\text{req'd-adj}}$? (OR calculate $f_v$ Is $f_v \leq F'_v$?)
         - Yes
         - Calculate $\Delta_{\text{max}}$ (no load factors!) using superpositioning and beam chart equations with the $I_x$ for the section.
           - $I_{\text{req'd}} \leq \frac{\Delta_{\text{no big}}}{\Delta_{\text{limit}}}$
           - This may be both the limit for live load deflection and total load deflection.
             - No pick a section with a larger $I_x$. (DONE)
             - Yes (DONE)
   - No pick a new section with a larger area.