Rigid and Braced Frames

Rigid Frames

Rigid frames are identified by the lack of pinned joints within the frame. The joints are rigid and resist rotation. They may be supported by pins or fixed supports. They are typically statically indeterminate.

Frames are useful to resist lateral loads.

Frame members will see
- shear
- bending
- axial forces

and behave like beam-columns.

Behavior

The relation between the joints has to be maintained, but the whole joint can rotate. The amount of rotation and distribution of moment depends on the stiffness (EI/L) of the members in the joint.

End restraints on columns reduce the effective length, allowing columns to be more slender. Because of the rigid joints, deflections and moments in beams are reduced as well.

Frames are sensitive to settlement because it induces strains and changes the stress distribution.

Types

Gabled – has a peak

Portal – resembles a door. Multi-story, multiple bay portal frames are commonly used for commercial and industrial construction. The floor behavior is similar to that of continuous beams.

Staggered Truss – Full story trusses are staggered through the frame bays, allowing larger clear stories.
Connections

*Steel* – Flanges of members are fully attached to the flanges of the other member. This can be done with welding, or bolted plates.

*Reinforced Concrete* – Joints are monolithic with continuous reinforcement for bending. Shear is resisted with stirrups and ties.

**Braced Frames**

Braced frames have beams and columns that are “pin” connected with bracing to resist lateral loads.

**Types of Bracing**

- knee-bracing
- diagonal (including eccentric)
- X
- K or chevron
- shear walls – which resist lateral forces in the plane of the wall

**Rigid Frame Analysis**

Structural analysis methods such as the *portal method* (approximate), the *method of virtual work*, *Castigliano’s theorem*, the *force method*, the *slope-displacement method*, the *stiffness method*, and *matrix analysis*, can be used to solve for internal forces and moments and support reactions.

Shear and bending moment diagrams can be drawn for frame members by isolating the member from a joint and drawing a *free body diagram*. The internal forces at the end will be equal and opposite, just like for connections in *pinned frames*. Direction of the “beam-like” member is usually drawn by looking from the “inside” of the frame.
Frame Design

The possible load combinations for frames with dead load, live load, wind load, etc. is critical to the design. The maximum moments (positive and negative) may be found from different combinations and at different locations. Lateral wind loads can significantly affect the maximum moments.

Plates and Slabs

If the frame is rigid or non-rigid, the floors can be a plate or slab (which has drop panels around columns). These elements behave differently depending on their supports and the ratio of the sides.

- one-way behavior: like a “wide” beam, when ratio of sides > 1.5
- two-way behavior: complex, non-determinate, look for handbook solutions

Floor Loading Patterns

With continuous beams or floors, the worst case loading typically occurs when alternate spans are loaded with live load (not every span). The maximum positive and negative moments may not be found for the same loading case! If you are designing with reinforced concrete, you must provide flexure reinforcement on the top and bottom and take into consideration that the maximum may move.
Example 1

The rigid frame shown has been analyzed using an advanced structural analysis technique. The reactions at support A are: \( A_x = 2.37 \text{ kN}, A_y = 21.59 \text{ kN}, M_A = -4.74 \text{ kN}\cdot\text{m} \). The reactions at support C are: \( C_x = -2.37 \text{ kN}, C_y = 28.4 \text{ kN}, M_C = -26.52 \text{ kN}\cdot\text{m} \). Draw the shear and bending moment diagrams, and identify \( V_{\text{max}} \) & \( M_{\text{max}} \).

Solution

Reactions These values must be given or found from non-static analysis techniques. The values are given with respect to the global coordinate system we defined for positive and negative forces and moments for equilibrium.

Member End Forces The free-body diagrams of all the members and joints of the frame are shown above. The unknowns on the members are drawn positive, and the opposite directions are drawn on the joint. We can begin the computation of internal forces with either member AB or BC, both of which have only three unknowns.

Member AB With the magnitudes of reaction forces at A know, the unknowns are at end B of \( \text{BA}_x, \text{BA}_y, \) and \( \text{M}_{\text{BA}} \), which can get determined by applying \( \sum F_x = 0, \sum F_y = 0, \) and \( \sum M_B = 0 \). Thus,
\[
\sum F_x = 2.37 \text{ kN} + \text{BA}_x = 0 \quad \text{BA}_x = -2.37 \text{ kN}, \quad \sum F_y = 21.59 \text{ kN} + \text{BA}_y = 0 \quad \text{BA}_y = -21.59 \text{ kN}
\]
\[
\sum M_B = 2.37 \text{ kN}(6\text{m}) - 4.74 \text{ kN}\cdot\text{m} + \text{M}_{\text{BA}} = 0 \quad \text{M}_{\text{BA}} = -9.48 \text{ kN} \cdot \text{m}
\]

Joint B Because the forces and moments must be equal and opposite, \( \text{BC}_x = 2.37 \text{ kN}, \text{BC}_y = 21.59 \text{ kN} \) and \( \text{M}_{\text{BC}} = 9.48 \text{ kN} \cdot \text{m} \)

Member BC All forces are known, so equilibrium can be checked:
\[
\sum F_x = 2.37 \text{ kN} - 2.37 \text{ kN} = 0 \quad \sum F_y = 21.59 \text{ kN} + 28.49 \text{ kN} - (10 \text{ kN} / \text{m})5\text{m} = 0
\]
\[
\sum M_B = 28.41 \text{ kN}(5\text{m}) - 10 \text{ kN} \cdot \text{m}(5\text{m})(2.5\text{m}) - 26.52 \text{ kN} \cdot \text{m} + 9.48 \text{ kN} \cdot \text{m} = 0
\]
Example 2

The rigid frame shown has been analyzed using an advanced structural analysis technique. The reactions at support A are: \( A_x = -28.6 \text{ k}, A_y = -15.3 \text{ k}, \) \( M_A = 208 \text{ k-ft} \). The reactions at support D are: \( D_x = -11.4 \text{ k}, D_y = 15.3 \text{ k}, \) \( M_D = 110 \text{ ft-k} \). Draw the shear and bending moment diagrams, and identify \( V_{\text{max}} \) & \( M_{\text{max}} \).

Solution:

\textit{NOTE: The joints are not shown, and the load at joint B is put on only one body.}